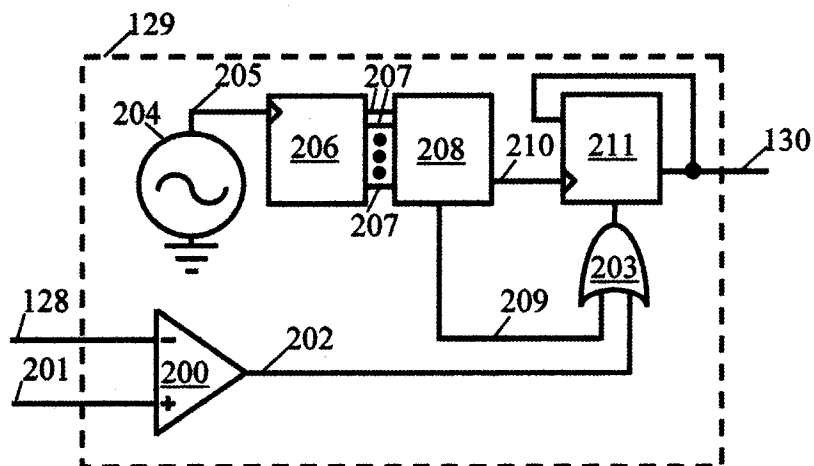
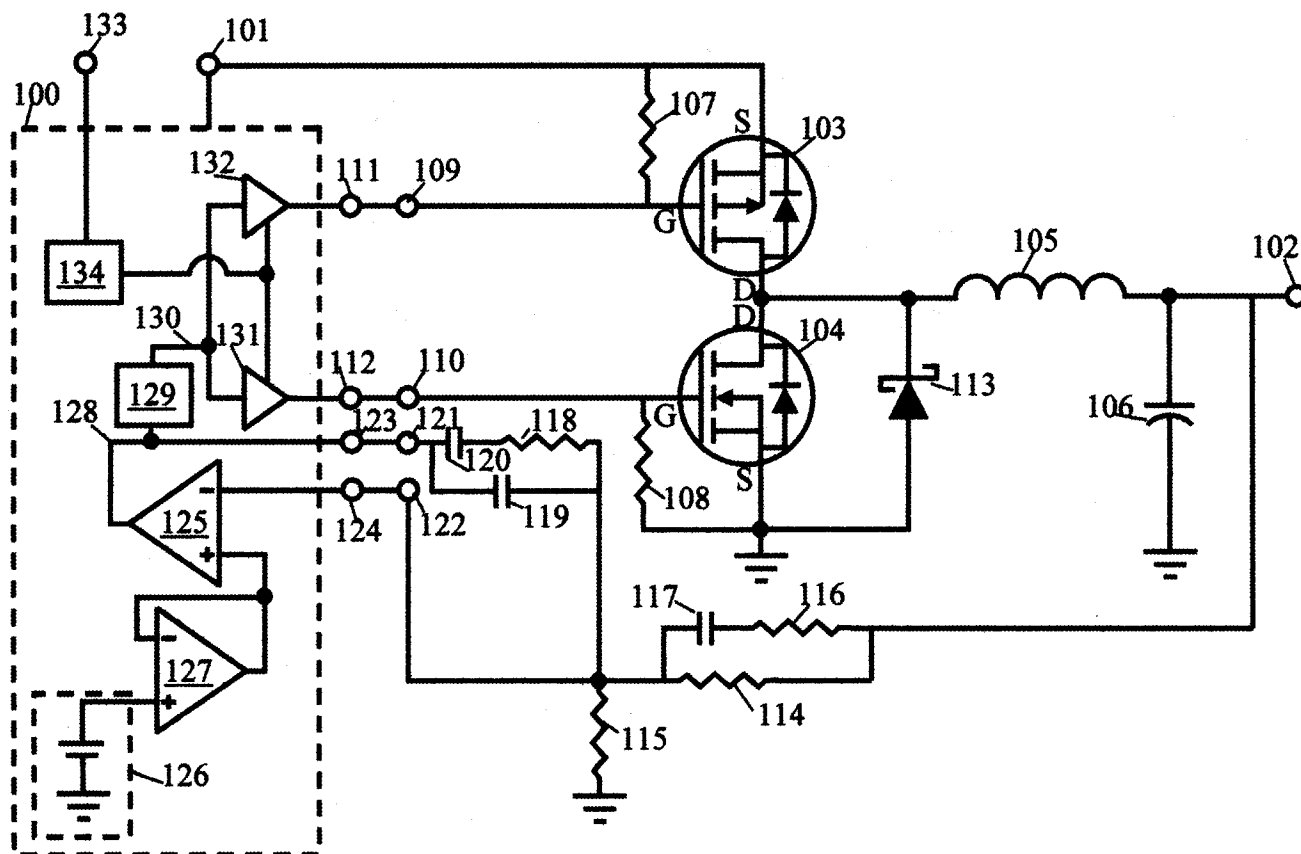


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**FIG. 2**

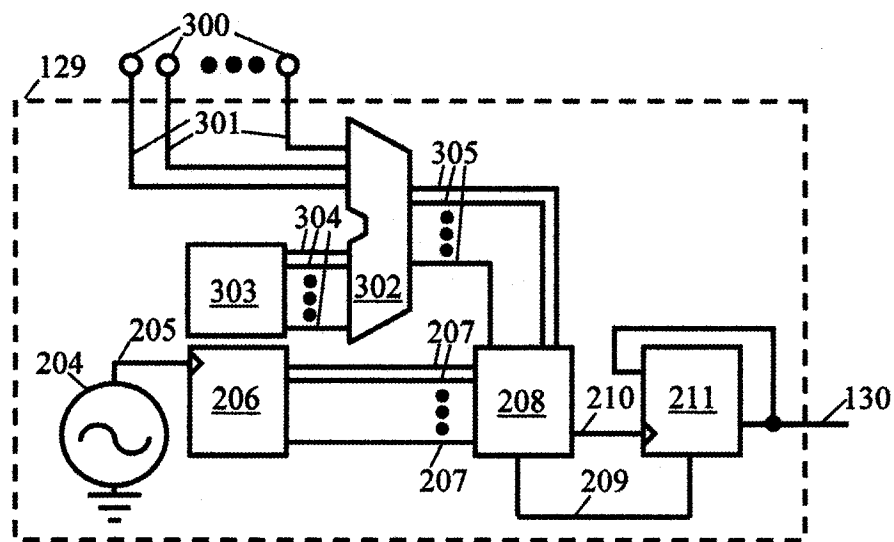


FIG. 3

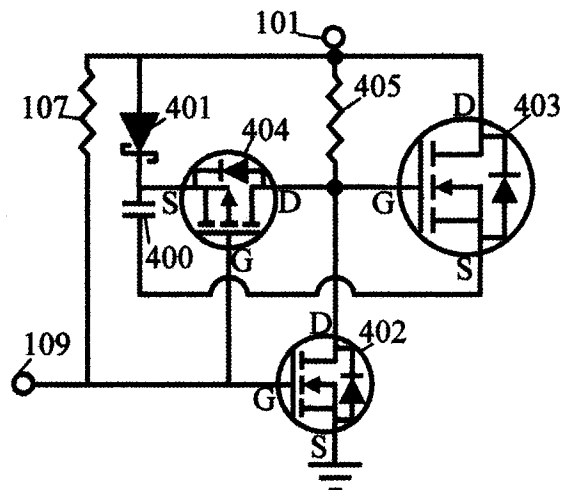


FIG. 4

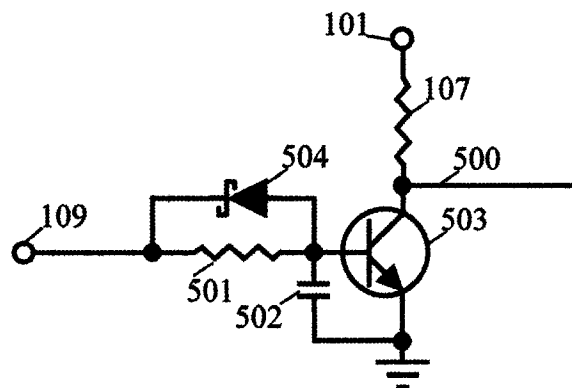
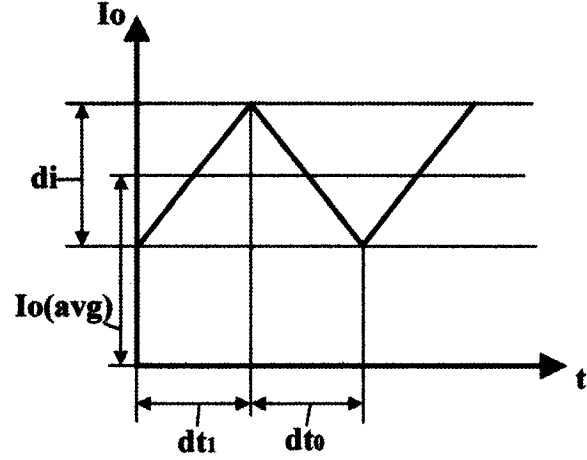
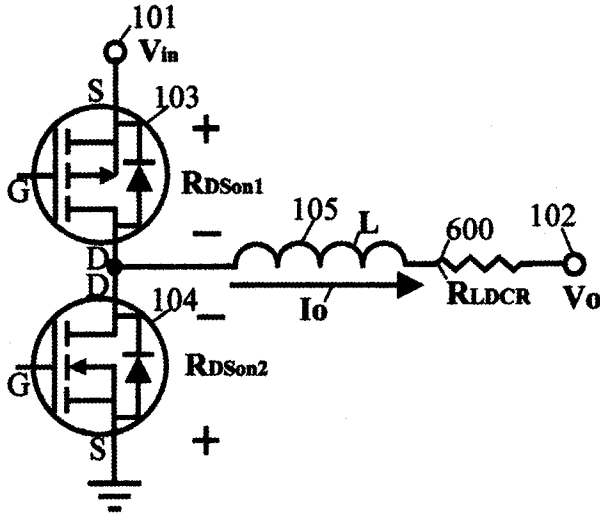


FIG. 5



**Kirchhoff's Voltage Law, 103 on, 104 off (dt1):**

**Kirchhoff's Voltage Law, 103 off, 104 on (dt0):**

$$0 = V_{in} - I_o(R_{DSon1} + R_{LDCR}) - L \frac{di}{dt_1} - V_o$$

$$0 = L \frac{di}{dt_0} - I_o(R_{DSon2} + R_{LDCR}) - V_o$$

$$\therefore V_o = V_{in} - I_o(R_{DSon1} + R_{LDCR}) - L \frac{di}{dt_1}$$

$$\therefore V_o = L \frac{di}{dt_0} - I_o(R_{DSon2} + R_{LDCR})$$

$$\therefore di = \frac{dt_1}{L} (V_{in} - V_o - I_o(R_{DSon1} + R_{LDCR})) \quad 602 \quad \therefore L \frac{di}{dt_0} = V_o + I_o(R_{DSon2} + R_{LDCR})$$

**Choose L, Fs such that  $di < 2(I_o(min))$  for continuous mode operation, (for this analysis to apply)**

$$\therefore V_o = V_{in} - I_o(R_{DSon1} + R_{LDCR}) - L \frac{di}{dt_1} = L \frac{di}{dt_0} - I_o(R_{DSon2} + R_{LDCR})$$

$$V_{in} = L di \left( \frac{1}{dt_1} + \frac{1}{dt_0} \right) + I_o(R_{DSon1} - R_{DSon2}) \quad \text{Switching Frequency} \equiv F_s = 1/(dt_1 + dt_0)$$

$$V_{in} = L di \left( \frac{dt_0 + dt_1}{dt_1(dt_0)} \right) + I_o(R_{DSon1} - R_{DSon2}) \quad \text{Duty Cycle} \equiv \delta = dt_1(F_s) \therefore dt_1 = \delta / F_s$$

$$V_{in} = L \frac{di}{dt_0} \left( \frac{1}{\delta} \right) + I_o(R_{DSon1} - R_{DSon2}) \therefore L \frac{di}{dt_0} = \delta(V_{in} - I_o(R_{DSon1} - R_{DSon2}))$$

$$L \frac{di}{dt_0} = \delta(V_{in} - I_o(R_{DSon1} - R_{DSon2})) = V_o + I_o(R_{DSon2} + R_{LDCR}) \quad 601$$

$$\therefore V_o = \delta(V_{in} - I_o(R_{DSon1} - R_{DSon2})) - I_o(R_{DSon2} + R_{LDCR})$$

**FIG. 6**

System and Method for Integrating a Digital Core With a Switch Mode Power Supply

Inventor: Andrew R. Gizara

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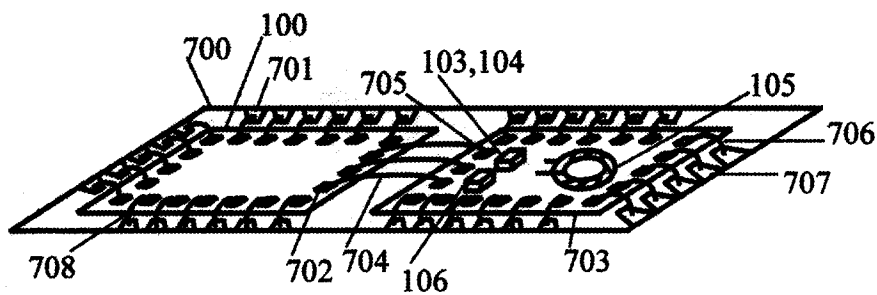


FIG. 7

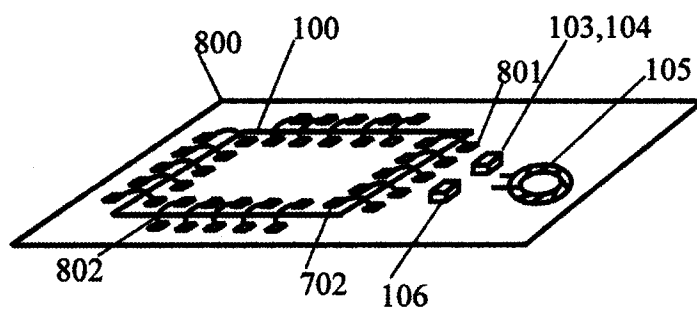


FIG. 8